

30 June 2014

Mr Adam Yacono Manager Anti-Dumping Commission C/o Australian Customs and Border Protection Service Customs House 1010 La Trobe Street DOCKLANDS VICTORIA 3008

Public File

Dear Mr Yacono

Hot Rolled Structural Sections (HRSS) exported from Japan, Korea, Taiwan and Thailand – Independent opinion on grade equivalents

OneSteel Manufacturing Pty Ltd ("OneSteel") submits that the central issue in the current HRSS investigation is the identification of the goods sold in the various domestic markets that most closely resemble the goods exported to Australia.

To assist in improving the understanding of the relevant criteria for identifying domestic grades that closely resemble AS/NZS 3679.1 -300 ("G300"), OneSteel has commissioned an independent assessor to prepare an expert report on the products most properly comparable with the exported G300 complying with AS/NZ 3679.1.

The independent expert report is attached for the Commission's guidance. The qualifications of the independent assessor are also included in the attachment.

Briefly, the independent assessment confirms that:

1. Based on mechanical properties

- The closest domestic grades of HRS to the exported G300 (compliant with AS/NZ 3679.1) include goods of Grade SM490A, SM490B and SM490C (to JIS G 3106), and SN490B and SN490C (to JIS G 3136).
- Grade SS400 is not even the closest to the redundant grade AS/3679.1 250 (G250"), let alone G300.
- Yield strength is a more important factor in evaluating design capacity of steel than tensile strength.

2. Based on chemical properties

- There is no equivalent for SS grades such as SS400 or SS490 as JIS G3101 doesn't specify limits for carbon equivalents.
- The closest domestic grades of HRS to the exported G300 (compliant with AS/NZ 3679.1) include goods of Grade SM490B and SM490C (to JIS G 3106), and SN490B and SN490C (to JIS G 3136). While these grades have the same requirement for the carbon equivalent, it is more difficult to achieve than the carbon equivalent for SM490A because of the less stringent limitation on carbon content in SM490A product.

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OneSteel submits that the independent assessment should provide the basis for preliminary dumping margin findings for Hyundai Steel Co, Tung Ho, TS Steel Co, Ltd, and Feng Hsin Iron and Steel Co., Ltd. The assessment will also impact yet-to-be-determined normal value assessments for SYS of Thailand.

If you have any questions concerning this letter please do not hesitate to contact OneSteel's representative Mr John O'Connor on (07) 3342 1921 or Mr Matt Condon of OneSteel on (02) 8424 9880.

Yours sincerely

Matt Condon Manager - Trade Development OneSteel Manufacturing Pty Ltd

Attachment - Independent Report



NZ Heavy Engineering Research Association Structural Systems

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Mr Matt Condon Manager Trade Development OneSteel Level 6, 205 Pacific Hwy St Leonards NSW 2065 Australia

30 June 2014

Dear Mr Condon

Equivalency of steel grades specified in JIS G 3101, JIS G 3106 and JIS G 3136 with AS/NZS 3679.1 Grades 250, 300 and 350

Synopsis

The present author has been working in the field of steel construction for over 20-years. As well as assisting Clients in Europe, the Middle East, Singapore and Australasia in research and product development activities, Stephen has a long experience of developing industry-standard design guidance as well as national and international Standards. Currently, he is General Manager of Structural Systems at the NZ Heavy Engineering Research Association (HERA); prior to him taking his present role, between 1997 and 2008, he was Senior Manager of Building Engineering at the Steel Construction Institute (SCI) in the UK. For complete details of the present author, a Curriculum Vitae is presented in Appendix C to this letter.

It is understood that independent expert advice is required on the equivalency of Japanese Industrial Standard (JIS) steel grades specified in JIS G 3101¹, JIS G 3106² and JIS G 3136³ compared to Grade 250 given in AS/NZS 3679.1: 1996⁴ together with Grades 300 and 350 given in AS/NZS 3679.1: 2010⁵.

JIS products equivalent to AS/NZS 3679.1 steel grades based on mechanical properties

To conform to the requirements given in AS/NZS 3679.1, test pieces produced according to AS 1391⁶ are required to establish the following key mechanical properties for the nominal thickness of the part from which the sample was taken:

- Minimum yield stress of the steel defined by the upper yield point R_{eH} expressed in MPa.
- Minimum tensile strength of the steel *R*_m expressed in MPa.
- Minimum elongation of the steel expressed as a percentage, reported on a gauge length L_0 equal to $5.65\sqrt{S_0}$ (known as a proportional test piece), where S_0 is the original cross-sectional area of the test piece before testing. Conversion of results from non-proportional test pieces is permitted using ISO 2566-1⁷ (i.e. when L_0 is not equal to $5.65\sqrt{S_0}$).

¹ JIS G 3101: 2010. Rolled steels for general structure, Japanese Standards Association, Tokyo, Japan, 2010

² JIS G 3106: 2008. Rolled steels for welded structure, Japanese Standards Association, Tokyo, Japan, 2008

³ JIS G 3136: 2012. Rolled steels for building structure, Japanese Standards Association, Tokyo, Japan, 2012

⁴ AS/NZS 3679.1: 1996. Structural Steel – Part 1: Hot-rolled Bars and Sections, Standards Australia/Standards New Zealand, Sydney/Wellington, Australia/New Zealand, 1996

⁵ AS/NZS 3679.1: 2010. Structural Steel – Part 1: Hot-rolled Bars and Sections, Standards Australia/Standards New Zealand, Sydney/Wellington, Australia/New Zealand, 2010

⁶ AS 1391: 2007. Metallic materials – Tensile testing at ambient temperature, Standards Australia, Sydney, Australia, 2007

⁷ ISO 2566-1:1984 Steel - Conversion of elongation values - Part 1: Carbon and low alloy steels, International Organization for Standardization, Geneva, Switzerland, 1984

For steel supplied to JIS G 3101, JIS G 3106 and JIS G 3136, the equivalent test piece standard that is required to determine the above mechanical properties is JIS Z 2201⁸. Given the similarities between AS 1391 and JIS Z 2201 (which appear to be because they are both based on ISO 6892-1⁹), equivalency between the different steel grades can be made by comparing the above key mechanical properties in the respective JIS standard and AS/NZS 3679.1. Comparisons of the impact energy for sub-grades are excluded from this study.

From a comparison of the above mechanical properties given in JIS G 3101, JIS G 3106 and JIS G 3136 (see Appendix A), it is concluded that the following products are closest to the steel grades given in AS/NZS 3679.1:

- AS/NZS 3679.1-250
 - JIS G 3101 SS490.
- AS/NZS 3679.1-300
 - $\circ~$ JIS G 3106 SM490A, SM490B and SM 490C (\leq 100 mm).
 - $\circ~$ JIS G 3136 SN490B and SN490C (\geq 16 mm).
- AS/NZS 3679.1-350
 - $\circ~$ JIS G 3106 SM490YA ($\leq~$ 100 mm), SM490YB ($\leq~$ 100 mm), SM520B ($\leq~$ 100 mm) and SM 520C ($\leq~$ 100 mm).

It should be noted that, although the above products are closest to the steel grades in AS/NZS 3679.1, in some cases, they are not directly equivalent owing to the fact that they do not comply with the minimum elongation requirements given in AS/NZS 3697.1 (see Appendix A).

The standard that is used to design steel structures in Australia is AS 4100¹⁰. Like it's international counterparts, to ensure that steel structures possess adequately ductility when loaded (i.e. they are not susceptible to brittle/sudden failure), the key mechanical properties identified above need to satisfy additional performance requirements to enable the products to be used in design (see Appendix A). In the vast majority of cases, the yield stress f_y (or R_{eH}) is used to evaluate the design capacity of steel members to support the design loads. The only exception to this rule is in the design of tension members where both the yield stress and tensile strength f_u (or R_m) is considered. However, in circumstances where the design capacity of tension members is based on f_u , the calculated design capacity is downrated in most international standards, reflecting the greater variability in f_u compared to f_v .

Weldability JIS products based on chemical composition

The present author's colleague, Dr Michail Karpenko (Manager of NZ Welding Centre at HERA and Member of the Standards Australia WD-003 Committee responsible for AS/NZS 1554.1¹¹ *et seq.*), has also considered the weldability based on the chemical composition of the JIS products. Weldability of steel is an important indicator for expected mechanical properties of the heat affected zone (HAZ) of a welded joint. It is essential to know weldability of the steel in order to develop a suitable welding procedure that includes preheat temperature, heat input and other relevant parameters. Weldability of Australian and New Zealand steel grades is defined in AS/NZS 1554.1 as a Weldability Group Number.

From the observations presented in Appendix B it is concluded that the following products are closest to the steel grades given in AS/NZS 3679.1:

• AS/NZS 3679.1-250

• No equivalency, as JIS G 3101 does not specify limits for carbon equivalent of SS490.

¹⁰ AS 4100: 1998. Steel structures, Standards Australia, Sydney, Australia, 1998

 ⁸ JIS Z 2201: 1998. Test pieces for tensile test for metallic materials, Japanese Standards Association, Tokyo, Japan, 1998
 ⁹ ISO 6892-1: 2009. Metallic materials - Tensile testing - Part 1: Method of test at room temperature, International Organization for Standardization, Geneva, Switzerland, 2009

¹¹ AS/NZS 1554.1: 2011. Structural steel welding - Welding of steel structures, Standards Australia/Standards New Zealand, Sydney/Wellington, Australia/New Zealand, 2011

• AS/NZS 3679.1-300

- JIS G 3106 SM490B (\leq 50 mm) and SM490C (\leq 100 mm).
- o JIS G 3136 SN490B (6 mm to 50 mm) and SN490C (16 mm to 50 mm).
- AS/NZS 3679.1-350
 - o JIS G 3106 SM490A, SM490B, SM490C, SM490YA, SM490YB, SM520B and SM520C
 - JIS G 3136 SN490B, SN490C

The basis for considering the above JIS grades to have similar weldability to AS/NZS 3679.1 grades above is from a conservative estimate of the maximum carbon equivalents (CE) based on chemical composition limits provided in the Japanese standards.

The equivalency of weldability of steels considered above is only valid for JIS grades with a maximum boron content of 0.0007%.

Conclusions

From the above review, taking both the mechanical properties and chemical composition into consideration, is concluded that the following products are closest to the steel grades given in AS/NZS 3679.1:

- AS/NZS 3679.1-300
 - JIS G 3106 SM490B (\leq 50 mm) and SM490C (\leq 100 mm).
 - o JIS G 3136 SN490B (6 mm to 50 mm) and SN490C (16 mm to 50 mm).

• AS/NZS 3679.1-350

JIS G 3106 SM490YA, SM490YB, SM520B and SM520C

Should you have any queries on the results from the work described in this letter, please do not hesitate to contact me.

Yours sincerely

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Dr Stephen Hicks General Manager Structural Systems E-Mail: <u>stephen.hicks@hera.org.nz</u>

Appendix A Detailed comparisons between JIS products equivalent to AS/NZS 3679.1 steel grades

To enable the conclusions presented in this letter to be independently reviewed, a comparison of the mechanical properties given in JIS G 3101, JIS G 3106 and JIS G 3136 with AS/NZS 3679.1 are presented in Table 1. The non-proportional values given in the JIS documents have been converted according to ISO 2566-1 to those based on a proportional gauge length, so that a direct comparison of the minimum elongation values can be made (see Fig. 1). As can be seen from Fig. 1, in some cases, the JIS grades do not comply with the minimum elongation requirements given in AS/NZS 3697.1 for a particular nominal thickness.

Table 1 Mechanical	properties at	ambient	temperature	according to	AS/NZS	3679.1,	JIS	G 3101,
JIS G 3106 and JIS C	G 3136			-				

Designation	Minimum yield stress R _{eH}					Minimum tensile	Minimum elongation on
	Nominal thickness					strength	a gauge
	mm					R _m	length of
	< 11	≥11	>16	>17	≥ 40	MPa	5.65√S₀
		≤16	≤17	<40			%
AS/NZS 3679.1-250	260	250	250	250	230	410	22
JIS G 3101 SS490	285	275	275	275	255†	490 to 610	See Fig. 1 ^a
AS/NZS 3679.1-300	320	300	300	280	280	440	22
JIS G 3106 SM490A	325	325	325	315	295†	490 to 610	See Fig. 1 ^b
JIS G 3136 SN490B	325	325‡	325	325	295†	490 to 610	See Fig. 1 [°]
JIS G 3136 SN490C	-	-	325	325	295†	490 to 610	See Fig. 1 ^d
AS/NZS 3679.1-350	360	340	340	340	330	480	20
JIS G 3106 SM490YA and	365	365	355	355	335†	490 to 610	See Fig. 1 ^e
SM490YB							
JIS G 3106 SM520B and	365	365	355	355	335†	520 to 640	See Fig. 1 ^e
SM520C							

Notes: † applies to > 40 mm, ‡ applies to \geq 12 mm and <16 mm

a Does not conform to minimum elongation of 22%

b Conforms to minimum elongation for nominal thickness of: ≥ 5.1 mm and ≤ 8.6 mm; and ≥ 16.1 mm and ≤ 24.8 mm

c Conforms to minimum elongation for nominal thickness of: ≥ 6 mm and ≤ 8.6 mm; and ≥ 16.1 mm and ≤ 24.8 mm

d Conforms to minimum elongation for nominal thickness of \geq 16.1 mm and \leq 24.8 mm

e Conforms to minimum elongation for nominal thickness of: \geq 5.1 mm and \leq 7.4 mm; and \geq 16.1 mm and \leq 24.2 mm



Fig 1 Elongation-nominal thickness relationship for JIS G 3101, JIS G 3106 and JIS G 3136 products compared to AS/NZS 3679.1

In order to ensure that structures designed to AS 4100 utilize steels that possess adequate ductility, the key variables identified in the body of the letter are used to satisfy the following requirements (in design R_{eH} is designated f_y , whilst R_m is designated f_u):

•
$$\frac{R_m}{R_{eH}} = \frac{f_u}{f_y} \ge 1.2$$

- elongation at failure \geq 15% (on a gauge length of 5.65 $\sqrt{S_o}$).
- the stress-strain curve for the steel has a plateau at f_y extending for at least $6\varepsilon_y$, where ε_y is the yield strain.
- the steel exhibits a strain-hardening capability.

In the vast majority of cases in design, the yield stress f_y (or R_{eH}) is used to evaluate the capacity of steel members. The only exception to this rule is in the design of tension members where the design section capacity is taken as the lesser of:

 $\phi N_t = \phi A_g f_v$; and

 $\phi N_t = 0.85 \phi k_t A_n f_u$

where ϕ is the capacity (safety) factor which is given as value of 0.9 in AS 4100, A_g is the gross area of the cross-section, k_t is the correction factor for distribution of forces, A_n is the net area of the cross-section (accounting for holes for, for example, fasteners) and f_u (or R_m) is the tensile strength used in design.

The factor 0.85 in the second of the above two equations ensures that the effective capacity factor 0.85ϕ (≈ 0.77) for the limit state of material fracture is suitably higher than the value of ϕ (=0.9) for the limit state of yielding, reflecting the influence of greater variability in f_u and the reduced ductility of members which fail by fracture at bolt holes.

Innovation in Metals

Appendix B Detailed review of the weldability of JIS products based on chemical composition

It is concluded that JIS G 3106 and JIS G 3136 apply the carbon equivalent equation C_{eq} , which is somewhat different to that used in AS/NZS 3679.1. Compared with C_{eq} , the Carbon Equivalent (CE) formula given in AS/NZS 3679.1 leads to more conservative results. However, the lower C_{eq} limits given for JIS G 3106-SM490 and JIS G 3136-SN400 appear to balance the difference in the carbon equivalent formulas. The crack sensitivity index, which also takes boron content into account, is not included in AS/NZS 3679.1.

It is not possible to accurately estimate the CE based on the chemical composition limits given in the JIS standards presently under consideration. As JIS steel grades are not listed in AS/NZS 1554.1, welding of these grades will require special considerations. To determine the pre-heat temperature, the weldability group number of the parent material should be identified based on the actual ladle analysis and the CE in accordance with Section 5.3 of AS/NZS 1554.1. Welding procedure qualification testing should comply with the Table 4.7.1 of AS/NZS 1554.1 or AS/NZS 1554.5, following the testing requirements for not pre-qualified welding consumables; this includes tensile, bend and impact tests. Material test certificates should report all elements listed in the CE formula plus total boron. For steels containing more than 0.0007% total boron, the weld heat affected zone (HAZ) Charpy testing should be considered in lieu of the parent plate Charpy tests.

JIS G 3106

JIS G 3106 gives the maximum value of the JIS Carbon Equivalent (C_{eq}) for SM 490A, SM 490YA, SM 490B SM 490YB SM 490C (SM490) grades as 0.38 max (50 mm plate thickness or under) and 0.4 max for (over 50 mm up to and incl. 100 mm). The C_{eq} for the steel plate over 100 mm in thickness is subject to the agreement between the purchaser and supplier.

The chemical composition of the steel shall be determined by the ladle analysis subject to an agreement between purchaser and supplier. The ladle analysis values of the Table 2, JIS G 3106 specify limits for five elements (C, Si, Mn, P and S) only. The maximum levels of S and P are more restrictive compared to AS/NZS 3679.1.

Sensitivity of Welding Crack Index (PCM) can be used as substitute for C_{eq} under the agreement between the purchaser and the supplier. Table 6, JIS G 3106 gives the maximum value of PCM for SM 490 grades as 0.24 max (50 mm plate thickness or under) and 0.26 max for (over 50 mm up to and including 100 mm). The PCM for the steel plate over 100 mm in thickness is subject to the agreement between the purchaser and supplier.

In contrast, AS/NZS 3679.1 specifies limits for some twelve elements including all those required to estimate Carbon Equivalent (CE). The maximum value of the carbon equivalent is given as CE 0.44 and 0.45 for the Grade 300 and 350 respectively. The corresponding weldability group number according to AS/NZS 1554.1 is 4 and 5.

JIS G 3136

JIS G 3136 gives the maximum values of the C_{eq} and PCM that should be calculated using actual heat analysis values. The standard specifies limits for five elements (C, Si, Mn, P and S) only. With the exception of the grade SN 400A, the maximum levels of S and P are more restrictive as compared to AS/NZS 3679.1.

JIS G 3101

JIS G 3101 species limits for four elements (C, Mn, P and S) only. It does not include C_{eq} formula. The maximum level of S and P are less restrictive for the Grades SS330, SS400, SS490 and SS540 as compared to AS/NZS 3679.1.

Appendix B Curriculum Vitae for Dr Stephen James Hicks



PERSONAL INFORMATION



Stephen James Hicks

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- http://www.linkedin.com/pub/stephen-hicks/25/825/b32
- Skype stephen hicks1

Sex Male | Date of birth 20/09/1969 | Nationality British

WORK EXPERIENCE

03/09/2012-Present

General Manager of Structural Systems

Heavy Engineering Research Association, Auckland (New Zealand)

As Manager plus:

Member of senior management team.

Business or sector Not-for-profit research organisation

09/07/2008-03/09/2012 Manager of Structural Systems

Heavy Engineering Research Association, Auckland (New Zealand)

Responsible for setting annual budget and financial forecast for the Structural Systems Division (annual turn-over NZ\$1.200.000); Responsible for divisional business development; Contribution to the overall strategic management of HERA through attendance of management and executive meetings; Staff management and appraisal of 5 researchers and business development experts; Authoring journal papers, industry design guides and chapters in books; Lecturing at Universities, seminars and teaching at Continuing Professional Development (CPD) courses in NZ, Australia and Asia; Responsible for consultancy activities; Responsible for structural testing and management of Universities and research institutes; Answering questions from designers and providing interpretations of clauses within Standards; PhD mentor and examiner; Member of NZ and Australian Standards Committees on steel and composite construction.

Business or sector Not-for-profit research organisation

11/2013-Present Director

Australasian Certification Authority for Reinforcing and Structural Steels (ACRS), Sydney (Australia)

Monitor business performance; Ensure financial viability and accountability; Act in accordance with ASIC company law; Develop with the Board and enact strategic policy and direction; Monitor the controls framework to ensure major risks are identified and managed; Develop alternative funding sources in conjunction with Board and management; Approve budgets, large investments and any major financial decisions; Appoint to the Executive Director and evaluate his or her performance.

Business or sector Conformity assessment body

Executive Councillor 09/2012-Present

Steel Construction New Zealand (SCNZ), Auckland (New Zealand)

As ACRS Director

Business or sector Steel construction marketing association

07/2008-Present Director

National Association of Steel-framed Housing (NASH), Auckland (New Zealand)



As ACRS Director

Business or sector Light steel framing marketing association

01/10/2007–03/06/2008 Senior Manager of Building Engineering

Steel Construction Institute (SCI), Ascot (United Kingdom)

As Manager plus:

Member of Senior Management team; Responsible for setting annual budget and financial forecast for the Building Engineering Division (annual turn-over £700.000); Responsible for divisional business development; Contribution to the overall strategic management of the Institute; Staff management and appraisal of Manager of Fire Engineering, Manager of Tubular Construction together with 3 Principal and Senior Engineers.

Business or sector Research organisation

01/10/2004–01/10/2007 Manager of Building Engineering

Steel Construction Institute (SCI), Ascot (United Kingdom)

As Principal Engineer plus:

Responsible for setting annual budget and financial forecast for the Building Engineering Sub-division (annual turn-over £600.000); Responsible for Sub-division business development; Staff management and appraisal of 3 Principal and Senior Engineers; Responsible for the development of consultancy service in evaluating floor vibrations using finite element analyses; UK Member on CEN/TC250/SC4 Eurocode 4; Reported directly to the SCI Director: Dr Graham W Owens

Business or sector Research organisation

01/04/1999–01/10/2004 Principal Engineer

Steel Construction Institute, Ascot (United Kingdom)

As Senior Engineer plus:

Responsible for financial control and management of selected projects; Responsible for business development and preparation of proposals for funding from RFCS, ECSC, UK DTI and UK DETR; Supervision of Engineers; Lecturing at Universities and Continuing Professional Development courses for designers; Member of national standards committee for composite construction BSI B/525/4.

Business or sector Research organisation

03/03/1997–01/04/1999 Senior Engineer

Steel Construction Institute, Ascot (United Kingdom)

Research and development of steel and steel-concrete composite structures in multi-storey buildings; Responsible for managing individual projects; Preparation of reports and delivering internal presentations; Finite element modelling and software programming; Supervision of structural testing and management of Universities and research institutes; Answering questions from designers and providing interpretations of clauses within Standards; Preparation of technical papers for journals and external audiences; Public speaking; Reported to Dr Mark Lawson, Senior Manager of the Building and Construction Division.

Business or sector Research organisation

01/06/1987–21/09/1990 Civil engineering technician

Packman Lucas, London (United Kingdom)

Producing structural design calculations for office and residential buildings in reinforced concrete, timber, masonry and steel; Site supervision; Preparation of briefs; Site surveying and ground investigation; Organizing work for drawing staff; Hand and Computer Aided Drafting (CAD).



Curriculum Vitae

Business or sector Structural engineers

EDUCATION AND TRAINING							
01/10/1993–21/03/1998	Doctor of Philosophy in Engineering (PhD)GBR DoctorateUniversity of Cambridge, Board of Graduate Studies4 Mill Lane UK-CB21RZ Cambridge (United Kingdom)						
	Title of dissertation: L	ongitudinal shear re	sistance of steel and	concrete composite	beams		
27/09/1990-01/08/1993	Bachelor of Engineering with First Class Honours (BEng(Hons)) GBR Bachelors degree						
	University of London, Mile End Road UK-E	Queen Mary and V 14NS London (Unite	/estfield College, De ed Kingdom)	partment of Civil Eng	ineering		
01/09/1988–01/06/1990	Business and Technology Education Council (BTEC) Higher National Certificate (HNC)GBR Higher National Certificate (HNC)Newham Community College East Ham Centre, High Street South UK-E64ER London (United Kingdom)GBR Higher National Certificate (HNC)						
01/09/1986–03/10/1988	Business and Technology Education Council (BTEC) National Certificate (NC)GBR BTEC National CertificateBarking College of Technology, Romford (United Kingdom)GBR BTEC National Certificate						
PERSONAL SKILLS							
Mother tongue(s)	English						
Other language(s)	UNDERSTANDING		SPEAKING		WRITING		
	Listening	Reading	Spoken interaction	Spoken production			
French	B2	B2	B1	B1	B2		
Communication skills	Levels: A1/A2: Basic user Common European Fram Good ability to adap	- B1/B2: Independent u: ework of Reference for to multicultural e	ser - C1/C2: Proficient us Languages environments, gaine	er ed through:			
	 i) My current position first joint Australian ar committee membersh ii) UK member on Eu Eurocode 4 - Design iii) Working with a wic Community (ECSC) a iv) Teaching and const 	in New Zealand, wh nd New Zealand ste nips for other Austra ropean Committee 1 of Composite Steel le variety of Europea and Research Fund sultancy activities in	hich has led me to se el and composite brid lian and New Zealan for Standardization, " and Concrete Struct an Universities and Ir for Coal and Steel (f China, Singapore ar	rve as Chairman of th dge design standard, d Standards. Structural Eurocodes ures (CEN/TC250/S0 nstitutions on Europe RFCS) research proje nd Bahrain	he committee for together with ", Subcommittee 4, C4). an Coal and Steel ects.		
	Strong verbal and personal communication gained through:						
	 a) Developing national and international Standards, authoring chapters in books, authoring national and international design guides and authoring journal papers. 						
	b) Delivering presenta Continuing Profession	ations to national an nal Development co	d international audie urses.	nces together with te	aching on		
Organisational / managerial skills	Leadership						
	 Staff management 	and appraisal					



Curriculum Vitae

- Technical and financial management
- Long track record of relationship building and business development.
- Extensive experience of working with key stakeholders in the UK, European and International steel construction industry
- Extensive experience of international collaborative research.

Job-related skills

 Technical and financial management.

- Steel and steel-concrete composite structures.
- Structural dynamics.
- National and international collaborative research.
- Standards development
- Negotiating and contractual relationships.
- Public speaking.
- Education and training development.
- Computer skills Good command of Microsoft Office[™] tools (e.g. Word[™], Excel[™] and PowerPoint[™]), including Visual Basic for Applications (VBA) programming.

Driving licence C1, D1, B, C1E, D1E, BE

ADDITIONAL INFORMATION

Honours and awards

- Invited to deliver 2014 annual lecture to the Singapore Structural Steel Society
 - Responsible for harmonizing New Zealand national standards for steel and composite construction with Australia and develop joint Australian/New Zealand design standards.
 - Only non UK-based individual to be considered a 'Eurocodes Expert' by the British Standards Institution, which resulted in the Eurocode 4 contribution to The Essential Guide to Eurocodes Transition book and the web-based Eurocodes Plus tool.
 - Led training on Eurocode 3 and 4 in three delegations to China (February 2012, July 2012 and March 2014).
- Invited by the Ministry of Housing, Bahrain to provide technical support for the introduction of light steel framing in residential buildings, Manama, Kingdom of Bahrain, 25 January 2010.
- Invited by European Commission Joint Research Centre to train the trainers from Member States on Eurocode 4 at: 'Eurocodes: Background and applications workshop', Brussels, 18-20 February 2008
- Engineering & Physical Sciences Research Council (EPSRC) Studentship Award 1994 to 1997.
- W.G. Collins Fund Award, Cambridge University Engineering Department 1996.
- The Institution of Civil Engineers Prize for Civil Engineering Students July 1993.

Participation on National and International Standards Committees

Australasia

- Member of Standards Australia BD-001 Committee: Steel Structures, from 2013 (responsible for steel structures design standard AS 4100 and fabrication and erection standard AS/NZS 109X and participation on ISO/TC167, ISO/TC167/SC1 and ISO/TC167/SC2)
- Member of Standards Australia BD-023 Committee: Structural Steel, from 2012 (responsible for steel product standards AS/NZS 1163, AS/NZS 3678, AS/NZS 3679.1 and AS/NZS 3679.2 and participation on ISO/TC17, ISO/TC17/SC3, ISO/TC71 and ISO/TC71/SC6)
- Member of Standards Australia BD-032 Committee: Composite Construction, from 2011 (responsible for design standards AS/NZS 2327.1, AS/NZS 2327.2, AS/NZS 2327.3 and AS/NZS 2327.4)
- Chairman of Standards Australia BD-032-4 Sub-Committee: Composite Construction -



Composite Slabs, from 2011 (responsible for design standard AS/NZS 2327.4)

- Member of Standards Australia BD-090 Committee: Bridge Design, from 2011, (responsible for Design standards AS 5100.1, AS 5100.2, AS 5100.3, AS 5100.4, AS 5100.5, AS/NZS 5100.6, AS 5100.7, AS 5100.8 and AS 5100.9)
- Chairman of Standards Australia BD-090-06 Sub-Committee: Bridge Design Steel and Composite Construction, from 2011 (responsible for design standard AS/NZS 5100.6)
- Member of Standards Australia MT-001 Committee: Iron and Steel, from 2010 (responsible for product standards AS 1397, AS 1448, AS 1444, AS 1450, AS 1442, AS 4738.1, AS 1447, AS 1448, AS 1830, AS 1831, AS 1832, AS 2027, AS 5052, AS 5054, AS 1988.1, AS 4314, AS 2338, AS 1443, AS 1770, AS 2074, AS 1472, AS 2266, AS/NZS 1594, AS 2423, AS 5049, AS 1833, AS 1394, HB 110.1, AS/NZS 1595, AS/NZS 4496, HB 12, HB 17, AS/NZS 1365, AS 1982, AS 2003, AS 1517, AS 2551, AS 2552 and AS 2028).
- New Zealand
 - □ **Member** of Standards New Zealand **P3404** Committee: Steel Structures, from 2008 (responsible for design standard NZS 3404.1)
- Europe
 - UK Member of European Committee for Standardization CEN/TC250/SC4 Subcommittee 4: Eurocode 4 - Design of Composite Steel and Concrete Structures, from 2005 to 2008 (responsible for EN 1994-1-1, EN 1994-1-2 and EN 1994-2).
- United Kingdom
 - Member of British Standards Institution B/525/04 Committee: Composite Structures, from 2003 to 2008 (responsible for UK National Annexes to EN 1994-1-1, EN 1994-1-2 and EN 1994-2 together with earlier National Standards, BS5950-3.1 and BS 5950-4).

Selected Collaborative Research	COST TU0904, Integrated Fire Engineering and Response, MC Observer, New Zealand, from 2011			
Projects	NZTA, TAR 09/08 Steel/Concrete Composite Bridge Design Guide, from March 2009 to September 2013			
	RFCS, RFS2-CT-2007-00033, Human-induced vibration of steel structures (Hivoss), from July 2007 to June 2008			
	RFCS, RFS2-CT-2005-00037, LWO+, large web openings for service integration in composites floors from July 2005 to December 2006			
	RFCS , ŘFSR-CT-2003-00025 , High quality acoustic and vibration performance of lightweight steel constructions, from September 2003 to December 2006			
	ECSC, 7210-PR/314, Generalisation of criteria for floor vibrations for industrial, office, residential and public building and gymnastic halls, from 1 July 2001 to 30 June 2004			
	ECSC, 7210-PR/315, Large web openings for service integration in composite floors, from 1 July 2001 to 31 December 2003			
	DTI, STBF/004/00053C, Holistic Assessment of the Vibration Sensitivity of Lightweight Floors for Various Use Patterns, from January 2004 to December 2005			
	DETR, 38/10/77 , Design of flooring systems using pre-cast concrete slabs supported by steel beams, from April 1999 to March 2002			
	DETR , 38/10/53, Design guidance & interpretation of Cardington composite frame tests, from March 1997 to September 1999.			
Memberships	Elected for a 4-year term on the International Association for Bridge and Structural Engineering Working Commission 2 (IABSE WC2): Steel Timber and Composite Structures from 2011			
	 Corresponding Member of European Convention for Constructional Steelwork Technical 			
	Committee 11 (ECCS TC 11): "Composite Structures", from 2011			
	Chairman of New Zealand Sustainable Steel Council, from 2009			
Publications - Books	El Sarraf, R, Iles, D, Momtahan, A, Easey, D and Hicks, S : Steel-concrete composite bridge design guide, 09/2013, New Zealand Transport Agency, ISBN: 9780478407693			



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Hicks, S.J., Lawson, R.M., Rackham, J.W. and Fordham, P: Comparative structure cost of modern commercial buildings. 01/2004; Steel Construction Institute., ISBN: 9781859421574

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